

入射面为  $x, z$  平面 ( $k_y^i = 0$ )

## 波动方程

对偶场

$\vec{E}$  &  $\vec{B}$

耦合关系

Maxwell 方程

解耦合

$\partial_z^2 \vec{E} = v^2(z) \nabla^2 \vec{E} + \text{边界条件}$

光源

入射光

波动方程

$\partial_z^2 \vec{E} = v^2(z) \nabla^2 \vec{E} + \vec{E}_i \cdot \theta(-z)$

1)

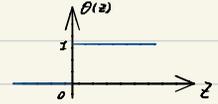
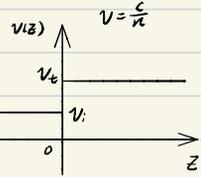
当  $z < 0$  时  $\partial_z^2 \vec{E} = \frac{c^2}{n_1^2} \nabla^2 \vec{E} + \vec{E}_i$

2)

当  $z > 0$  时  $\partial_z^2 \vec{E} = \frac{c^2}{n_2^2} \nabla^2 \vec{E}$

3)

当  $z = 0$  时  $\begin{cases} \vec{E}_{x,y}(z=0^+) = \vec{E}_{x,y}(z=0^-) \\ \vec{B}_{x,y}(z=0^+) = \vec{B}_{x,y}(z=0^-) \end{cases}$



电场切向连续

$\mu_1 = \mu_2 = 1$

## 波函数

预解式

$\vec{E} = (\vec{E}_i + \vec{E}_r) \cdot \theta(-z) + \vec{E}_t \cdot \theta(z)$

代入波动方程

验证解的形式, 求解解的参数

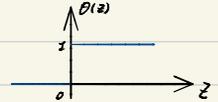
$z < 0$  预解式成立, 且  $\frac{\omega_r}{|k_r|} = \frac{c}{n_1}$

$z > 0$  预解式成立, 且  $\frac{\omega_t}{|k_t|} = \frac{c}{n_2}$

$z = 0 \begin{cases} \vec{E}_{x,y}(z=0^+) = \vec{E}_{x,y}(z=0^-) \Rightarrow \vec{E}_i^{x,y}(z=0) + \vec{E}_r^{x,y}(z=0) = \vec{E}_t^{x,y}(z=0) \\ \vec{B}_{x,y}(z=0^+) = \vec{B}_{x,y}(z=0^-) \Rightarrow \vec{B}_i^{x,y}(z=0) + \vec{B}_r^{x,y}(z=0) = \vec{B}_t^{x,y}(z=0) \end{cases}$

↓

$$\begin{cases} \omega_i = \omega_r = \omega_t & \text{同频, 同色} \\ k_i^y = k_r^y = k_t^y = 0 & \text{共面} \\ k_i^x = k_r^x = k_t^x & \text{波矢匹配条件} \\ E_i^x + E_r^x = E_t^x, E_i^y + E_r^y = E_t^y \\ B_i^x + B_r^x = B_t^x, B_i^y + B_r^y = B_t^y \end{cases}$$



物理性质 (方向, 强度)

波的传播方向

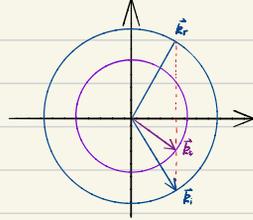
Snell's Law

$$w_i = w_r = w_t \quad k_i^y = k_r^y = k_t^y = 0 \quad k_i^x = k_r^x = k_t^x$$

$$\begin{cases} w_i = w_r = w_t \Rightarrow \frac{|k_i|}{n_i} = \frac{|k_r|}{n_r} = \frac{|k_t|}{n_t} \\ k_i^x = k_r^x = k_t^x \Rightarrow |k_i| \sin \theta_i = |k_r| \sin \theta_r = |k_t| \sin \theta_t \end{cases}$$

$$\Rightarrow \begin{cases} n_i \sin \theta_i = n_r \sin \theta_r \Rightarrow \theta_i = \theta_r \quad (\text{折射}) \\ n_i \sin \theta_i = n_t \sin \theta_t \Rightarrow \text{Snell's Law (反射)} \end{cases}$$

等波矢面法



$$|k_i| = |k_r| = \frac{w_i n_i}{c}$$

$$|k_t| = \frac{w_t n_t}{c}$$

全反射

等波面法表示  
解析表示

当  $|k_i| \sin \theta_i > |k_t| \Rightarrow \sin \theta_i > \frac{|k_t|}{|k_i|} = \frac{n_t}{n_i}$  时发生全反射

$$\vec{E}_t = \vec{E}_0^i e^{i(k_i^x x + k_i^y y - w_i t)}$$

$$\left. \begin{aligned} k_t^x &= k_i^x \\ (k_t^x)^2 + (k_t^z)^2 &= \frac{w_i^2 n_t^2}{c^2} \end{aligned} \right\} \Rightarrow k_t^z = \sqrt{\frac{w_i^2 n_t^2}{c^2} - (k_i^x)^2}$$

当  $k_i^x > |k_i| = \frac{w_i n_i}{c}$  时,  $k_t^z$  为虚数

波函数变为  $\vec{E}_t = \vec{E}_0^i e^{i(k_i^x x - w_i t)} e^{-\sqrt{(k_i^x)^2 - \frac{w_i^2 n_t^2}{c^2}} z}$  沿 z 方向 e 指数衰减

△ 全反射并非没有折射, 而是折射光的强度沿 z 轴指数衰减

受阻的全反射

光纤

光纤1 光纤2



光纤1中的光向光纤2中泄漏

# 光的强度

## 原则

Fresnell's Law 菲涅尔定律  
利用电场和磁场的边界条件

$$\text{电场} \begin{cases} \vec{n} \times (\vec{E}_i - \vec{E}_t) = 0 \\ \vec{n} \cdot (\vec{D}_i - \vec{D}_t) = \rho_f \end{cases} \quad \text{磁场} \begin{cases} \vec{n} \cdot (\vec{B}_i - \vec{B}_t) = 0 \\ \vec{n} \times (\vec{H}_i - \vec{H}_t) = \vec{K}_f \end{cases}$$

## 特殊情形①

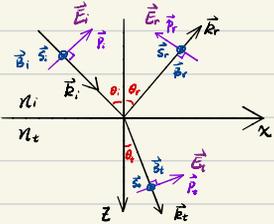
TM mode  $\vec{B} = (0, B_y, 0)$   $\vec{E} = |E| \hat{p}$

$$\text{边界条件: } \begin{cases} E_i^x + E_r^x = E_t^x \Rightarrow |E_i| \cos \theta_i - |E_r| \cos \theta_r = |E_t| \cos \theta_t \\ B_i^y + B_r^y = B_t^y \Rightarrow |B_i| + |B_r| = |B_t| \end{cases}$$

$$E-B \text{ 关系: } |B_i| = \frac{|E_i|}{v_i} = \frac{|E_i| n_i}{c} \quad |B_r| = \frac{|E_r| n_i}{c} \quad |B_t| = \frac{|E_t| n_t}{c}$$

$$\text{Snell 定律: } n_i \sin \theta_i = n_t \sin \theta_t \quad \theta_i = \theta_t$$

$$\frac{|E_r|}{|E_i|} = \frac{n_t \cos \theta_i - n_i \cos \theta_t}{n_i \cos \theta_i + n_t \cos \theta_t} \quad \frac{|E_t|}{|E_i|} = \frac{2 n_i \cos \theta_i}{n_i \cos \theta_i + n_t \cos \theta_t}$$



## 特殊情形②

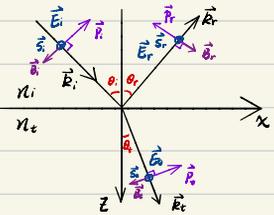
TE mode  $\vec{E} = (0, E_y, 0)$   $\vec{B} = |B| (-\hat{p})$

$$\text{边界条件: } \begin{cases} E_i^y + E_r^y = E_t^y \Rightarrow |E_i| + |E_r| = |E_t| \\ (\mu \approx 1) \quad B_i^x + B_r^x = B_t^x \Rightarrow -|B_i| \cos \theta_i + |B_r| \cos \theta_r = -|B_t| \cos \theta_t \end{cases}$$

$$E-B \text{ 关系: } |B_i| = \frac{|E_i|}{v_i} = \frac{|E_i| n_i}{c} \quad |B_r| = \frac{|E_r| n_i}{c} \quad |B_t| = \frac{|E_t| n_t}{c}$$

$$\text{Snell 定律: } n_i \sin \theta_i = n_t \sin \theta_t \quad \theta_i = \theta_t$$

$$\frac{|E_r|}{|E_i|} = \frac{n_t \cos \theta_i - n_i \cos \theta_t}{n_i \cos \theta_i + n_t \cos \theta_t} \quad \frac{|E_t|}{|E_i|} = \frac{2 n_i \cos \theta_i}{n_i \cos \theta_i + n_t \cos \theta_t}$$

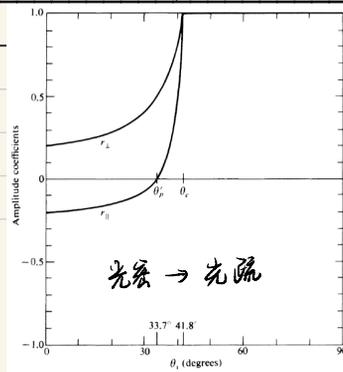
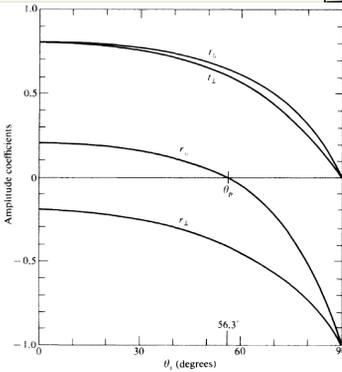


## 小结

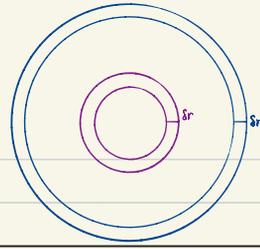
$$\text{令 } m = \frac{\cos \theta_t}{\sin \theta_i} \quad p = \frac{n_t}{n_i}$$

	TM ( $\hat{p}$ 分量)	TE ( $\hat{s}$ 分量)
振幅反射率	$r_p = \frac{p-m}{p+m}$	$r_s = \frac{1-pm}{1+pm}$
振幅透射率	$t_p = \frac{2}{p+m}$	$t_s = \frac{2}{1+pm}$

光疏  $\rightarrow$  光密



光密  $\rightarrow$  光疏

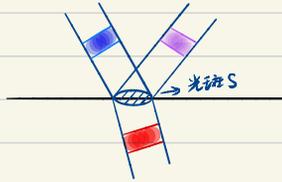


## 能量守恒

物理背景

物理系统

在  $t$  时刻沿向某一体积内的光能传播到  $t + \delta t$  后, 能量不变



$t$  时刻的体积



$t + \delta t$  时刻在反射光



$t + \delta t$  时刻在折射光

## 求解

① 求  $V(t)$  和  $V(t + \delta t)$

$$V_i(t) = S_i h_i = S h_i \cos \theta_i$$

$$V_r(t + \delta t) = S_r h_r = S h_r \cos \theta_r$$

$$V_t(t + \delta t) = S_t h_t = S h_t \cos \theta_t$$

$$\begin{cases} \frac{h_i}{v_i} = \frac{h_r}{v_r} = \frac{h_t}{v_t} \\ v = \frac{c}{n} \end{cases}$$

$$\Rightarrow n_i h_i = n_r h_r = n_t h_t$$

② 求电磁场能量密度

$$P_i = \frac{\varepsilon_0 E_i^2}{2} + \frac{1 B_i^2}{2} = \varepsilon_0 E_i^2 = \frac{n_i^2}{c^2} |E_i|^2$$

$$P_r = \varepsilon_0 E_r^2 = \frac{n_r^2}{c^2} |E_r|^2 = \frac{n_r^2}{c^2} r^2 |E_i|^2$$

$$P_t = \varepsilon_0 E_t^2 = \frac{n_t^2}{c^2} |E_t|^2 = \frac{n_t^2}{c^2} t^2 |E_i|^2$$

③ 验证  $U_i(t) = U_r(t + \delta t) + U_t(t + \delta t)$

$$U_i(t) = P_i V_i(t) = \frac{n_i^2}{c^2} |E_i|^2 \cdot S h_i \cos \theta_i = \frac{n_i h_i}{c^2} S |E_i|^2 \cdot n_i \cos \theta_i = I_i \cos \theta_i$$

$$U_r(t + \delta t) = P_r V_r(t + \delta t) = \frac{n_r^2}{c^2} r^2 |E_i|^2 \cdot S h_r \cos \theta_r = \frac{n_r h_r}{c^2} S |E_i|^2 \cdot r^2 n_r \cos \theta_r = I_r \cos \theta_r$$

$$U_t(t + \delta t) = P_t V_t(t + \delta t) = \frac{n_t^2}{c^2} t^2 |E_i|^2 \cdot S h_t \cos \theta_t = \frac{n_t h_t}{c^2} S |E_i|^2 \cdot t^2 n_t \cos \theta_t = I_t \cos \theta_t$$

$$I_i \cos \theta_i = I_r \cos \theta_r + I_t \cos \theta_t$$

$$\text{强度反射率 } R = \frac{I_r}{I_i} = r^2$$

$$\text{强度透射率 } T = \frac{I_t}{I_i} = \frac{n_t}{n_i} t^2$$

表 6-1 各种反射率和透射率的定义

	p 分量	s 分量
振幅反射率	$\tilde{r}_p = \tilde{E}'_{1p} / \tilde{E}_{1p}$ (6.13)	$\tilde{r}_s = \tilde{E}'_{1s} / \tilde{E}_{1s}$ (6.14)
强度反射率	$R_p = \frac{I'_{1p}}{I_{1p}} =  \tilde{r}_p ^2$ (6.15)	$R_s = \frac{I'_{1s}}{I_{1s}} =  \tilde{r}_s ^2$ (6.16)
能流反射率	$\mathcal{R}_p = \frac{W'_{1p}}{W_{1p}} = R_p$ (6.17)	$\mathcal{R}_s = \frac{W'_{1s}}{W_{1s}} = R_s$ (6.18)
振幅透射率	$\tilde{t}_p = \tilde{E}_{2p} / \tilde{E}_{1p}$ (6.19)	$\tilde{t}_s = \tilde{E}_{2s} / \tilde{E}_{1s}$ (6.20)
强度透射率	$T_p = \frac{I_{2p}}{I_{1p}} = \frac{n_2}{n_1}  \tilde{t}_p ^2$ (6.21)	$T_s = \frac{I_{2s}}{I_{1s}} = \frac{n_2}{n_1}  \tilde{t}_s ^2$ (6.22)
能流透射率	$\mathcal{T}_p = \frac{W_{2p}}{W_{1p}} = \frac{\cos i_2}{\cos i_1} T_p$ (6.23)	$\mathcal{T}_s = \frac{W_{2s}}{W_{1s}} = \frac{\cos i_2}{\cos i_1} T_s$ (6.24)

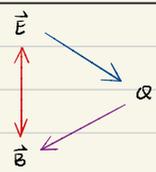
金属的折射和反射

波动方程

对偶场

解耦合

求解波函数



M3  $\nabla \times \vec{E} = -\frac{\partial \vec{B}}{\partial t}$   
 欧姆定律  $\vec{J} = \sigma \vec{E}$   
 M4  $\nabla \times \vec{B} = \mu(\vec{J} + \epsilon \frac{\partial \vec{E}}{\partial t})$

$$\left. \begin{aligned} \nabla \times \vec{E} &= -\frac{\partial \vec{B}}{\partial t} \\ \nabla \times \vec{B} &= \mu(\vec{J} + \epsilon \frac{\partial \vec{E}}{\partial t}) \end{aligned} \right\} \Rightarrow \left. \begin{aligned} \epsilon \mu \partial_t^2 \vec{E} &= \nabla^2 \vec{E} - \mu \partial_t \vec{J} \\ \vec{J} &= \sigma \vec{E} \end{aligned} \right\}$$

$\Rightarrow \epsilon \mu \partial_t^2 \vec{E} = \nabla^2 \vec{E} - \mu \sigma \partial_t \vec{E}$  耗散项

试探解  $E = E_0 e^{i(\vec{k} \cdot \vec{r} - \omega t)}$

代入波动方程  $-\omega^2 \epsilon \mu \vec{E} = -k^2 \vec{E} + \mu \sigma (i\omega) \vec{E}$

$\Rightarrow k^2 = \omega^2 (\epsilon \mu + \frac{i\mu\sigma}{\omega})$

$\Rightarrow n^2 = \frac{c^2}{v^2} = c^2 \frac{k^2}{\omega^2} = 1 + \frac{i\sigma}{\epsilon \omega}$

物理性质

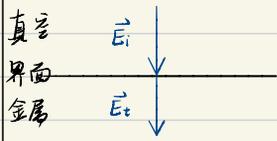
金属中的相速度

金属中的折射率

趋肤深度

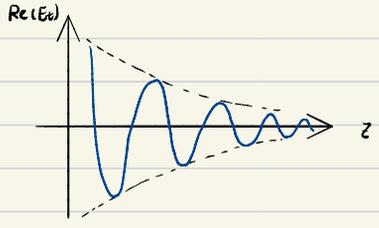
$v_p = \frac{\omega}{|k|} = \sqrt{\epsilon \mu + \frac{i\mu\sigma}{\omega}}$

$n = \sqrt{1 + \frac{i\sigma}{\epsilon \omega}}$

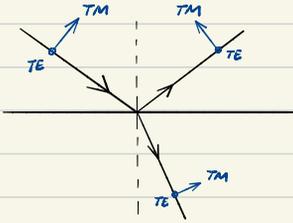


垂直入射时  $E_t = E_0 e^{i k_1 z} e^{-k_2 z}$   
 $I = I_0 e^{-2k_2 z}$

$\delta = \frac{1}{2} k I = \frac{1}{\sqrt{2\omega \mu \sigma}}$



# 折射 & 反射回顾



# 琼斯矢量 & 矩阵的描述

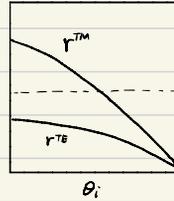
入、反、折射光的 J-矢量  $\begin{bmatrix} E_i^{TM} \\ E_i^{TE} \end{bmatrix}_\lambda \oplus \begin{bmatrix} E_r^{TM} \\ E_r^{TE} \end{bmatrix}_R \oplus \begin{bmatrix} E_t^{TM} \\ E_t^{TE} \end{bmatrix}_T$

折射 & 反射: J-矩阵

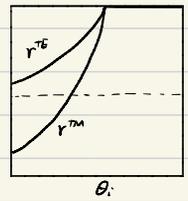
$$\begin{bmatrix} E_r^{TM} \\ E_r^{TE} \end{bmatrix} = \begin{bmatrix} r_{TM} & 0 \\ 0 & r_{TE} \end{bmatrix} \begin{bmatrix} E_i^{TM} \\ E_i^{TE} \end{bmatrix} \quad \begin{bmatrix} E_t^{TM} \\ E_t^{TE} \end{bmatrix} = \begin{bmatrix} t_{TM} & 0 \\ 0 & t_{TE} \end{bmatrix} \begin{bmatrix} E_i^{TM} \\ E_i^{TE} \end{bmatrix}$$

# S-定律 & F-公式

疏  $\Rightarrow$  密



密  $\Rightarrow$  疏



F-公式

S-定律 & F-公式适用所有平面波情形

# 折射 & 反射 $\Rightarrow$ 偏振

概括

① 利用 B-角入射产生 / 检测偏振光  $\Rightarrow$  偏振光

② 利用全反射调节偏振光  $\Rightarrow$  波片

利用 B-角 (布鲁斯特角) 做偏振片

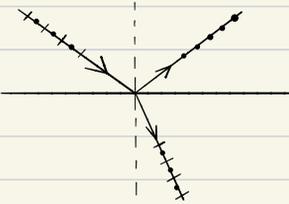
# B-角入射的回顾

定性描述

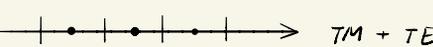
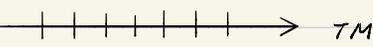
B-角入射  $\Rightarrow$   $\begin{cases} \text{反射光是纯 TE 光} \\ \text{透射光是 TM + TE 光} \end{cases}$

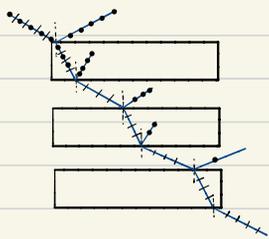
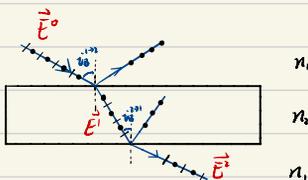
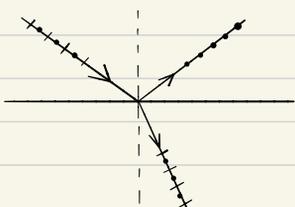
琼斯矢量 J-m  $\begin{bmatrix} E_i^{TM} \\ E_i^{TE} \end{bmatrix}_\lambda \Rightarrow \begin{bmatrix} 0 \\ r_{TE} E_i^{TE} \end{bmatrix}_R + \begin{bmatrix} t_{TM} E_i^{TM} \\ t_{TE} E_i^{TE} \end{bmatrix}_T$

$$\vec{J}_{\text{反射}} = \begin{bmatrix} 0 & 0 \\ 0 & r \end{bmatrix} \quad \vec{J}_{\text{透射}} = \begin{bmatrix} t_{TM} & 0 \\ 0 & t_{TE} \end{bmatrix}$$



# 画图约定





## 定量描述 (计算 $\theta_t$ )

出发点: Snell 定律 & Fresnel 公式

关系①  $r_{TM} = r_{TE} = \frac{P-m}{P+m} = 0 \Rightarrow P = m$

$$P = \frac{n_t}{n_i} \quad m = \frac{\cos \theta_t}{\cos \theta_i}$$

$$\Rightarrow \frac{\cos \theta_t}{\cos \theta_i} = \frac{n_t}{n_i} = \frac{\sin \theta_i}{\sin \theta_t} \Rightarrow \sin \theta_t \cos \theta_t = \sin \theta_i \sin \theta_t$$

$$\Rightarrow \sin 2\theta_t = \sin 2\theta_i \Rightarrow \theta_t = \frac{\pi}{2} - \theta_i = \frac{\pi}{2} - \theta_i$$

B-角入射时,  $\theta_t$  和  $\theta_i$  互余

关系②  $\sin^2 \theta_B = \frac{n^2}{n_i^2 + n_t^2} \Rightarrow \theta_B^{(n_i)} + \theta_B^{(n_t)} = \frac{\pi}{2}$

## 单层界面

$$\vec{J}_R = \begin{bmatrix} 0 & 0 \\ 0 & r_{TE} \end{bmatrix} \quad \vec{J}_T = \begin{bmatrix} t_{TM} & 0 \\ 0 & t_{TE} \end{bmatrix}$$

## 双层界面

偏振片

描述: 从  $n_1 \rightarrow n_2$  以  $\theta_i$  入射时, 在第二个界面入射角恰等于  $\theta_B^{(n_2)}$   
经过两次折射, 透射光中 TE 模式进一步减少

$$\vec{E}^2 = \vec{J}_{T2} \vec{E}^1 = \vec{J}_{T2} \vec{J}_{T1} \vec{E}^i$$

$$\Rightarrow \vec{J}_{T2} = \vec{J}_{T1} \cdot \vec{J}_{T2} \quad (\text{类似 ABCD 矩阵})$$

证明

$$\vec{J}_{T2} = \begin{bmatrix} t_{12}^{TM} & 0 \\ 0 & t_{12}^{TE} \end{bmatrix} \begin{bmatrix} t_{23}^{TM} & 0 \\ 0 & t_{23}^{TE} \end{bmatrix} = \begin{bmatrix} t_{12}^{TM} t_{23}^{TM} & 0 \\ 0 & t_{12}^{TE} t_{23}^{TE} \end{bmatrix}$$

小于单层膜

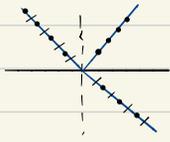
$t_{12}^{TE} \cdot t_{23}^{TE} \ll t_{12}^{TE}$  经过两层膜之后, 透射光中的 TE 模式  $\downarrow$

## 多层膜

经过多层膜 B-角反射 & 折射

反射光纯 TE 透射光纯 TM

$$\vec{J}_R = \begin{bmatrix} 0 & 0 \\ 0 & 1 \end{bmatrix} \quad \vec{J}_T = \begin{bmatrix} 1 & 0 \\ 0 & 0 \end{bmatrix}$$



小结

$$\vec{V}_r = \begin{bmatrix} 0 & 0 \\ 0 & r_2 \end{bmatrix}$$

$$\vec{V}_t = \begin{bmatrix} t_1 & 0 \\ 0 & t_1 \end{bmatrix}$$

入射光	单层		多层	
	t	r	t	r
线偏	线	线 (TE)	线 (TM)	线 (TE)
圆偏	椭			
椭偏	椭			
自然光	部分偏振			

利用全反射做波片

全反射回厥

全反射时  $|r_{11}| = |r_{21}| = 1$   $r_{11} = e^{i\phi_1}$   $r_{21} = e^{i\phi_2}$

光  $\rightarrow$  光

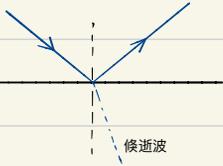
证明: S-定律  $\Rightarrow n_t \sin \theta_t = n_i \sin \theta_i$   $\sin \theta = \frac{e^{i\theta} - e^{-i\theta}}{2i}$

发生全反射时  $\sin \theta_t = \frac{n_i \sin \theta_i}{n_t} > 1$  ( $\theta_t$  是虚数)

F-公式  $\Rightarrow r_{11} = \frac{P-m}{P+m}$  可证  $r_{11} r_{11}^* = 1$   $|r_{11}| = 1$

同理  $|r_{21}| = 1$  且  $r_{11}$  和  $r_{21}$  为复数

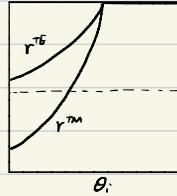
$$r_{11} = e^{i\phi_1} \quad r_{21} = e^{i\phi_2}$$



光密

光疏

候逝波



$\theta$

偏振调节

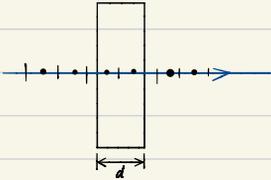
$$\vec{V}_r = \begin{bmatrix} r_{11} & 0 \\ 0 & r_{21} \end{bmatrix} \xrightarrow{\text{全反射}} \begin{bmatrix} e^{i\phi_1} & 0 \\ 0 & e^{i\phi_2} \end{bmatrix} = e^{i\phi_1} \begin{bmatrix} 1 & 0 \\ 0 & e^{i(\phi_2 - \phi_1)} \end{bmatrix}$$

$$= e^{i\phi_1} \begin{bmatrix} 1 & 0 \\ 0 & e^{i\phi} \end{bmatrix}$$

M和TE模式的光在全反射时, 有不同的相位效果 (波片)

$$\begin{bmatrix} E_r^{TM} \\ E_r^{TE} \end{bmatrix} = \vec{V}_r \begin{bmatrix} E_i^{TM} \\ E_i^{TE} \end{bmatrix} = e^{i\phi_1} \begin{bmatrix} E_i^{TM} \\ e^{i\phi} E_i^{TE} \end{bmatrix}$$

$$\underline{J}_{\text{波}} = e^{i\phi} \begin{bmatrix} 1 & 0 \\ 0 & e^{i\phi} \end{bmatrix}$$



### 波片

功能：对两个互相垂直的偏振方向，诱导不同的相位延迟

特征指标：**快轴**

对于TM, TE模式的光，相位积累(光程)少的轴是快轴

考虑一个波片，波片中  $v_{TE} > v_{TM} \Rightarrow k_{TE} < k_{TM}$  ( $v = \frac{c}{k}$ )

光程  $\phi_{TE} = k_{TE} d < k_{TM} d = \phi_{TM}$

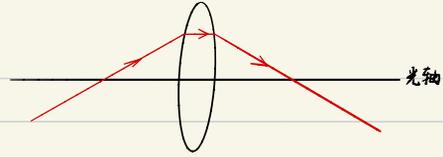
e.g. 若快轴为TE轴，则  $\phi_{TM} > \phi_{TE}$   $\Delta\phi = \phi_{TM} - \phi_{TE} > 0$

$$\underline{J} = e^{i\phi} \begin{bmatrix} 1 & 0 \\ 0 & e^{i(\phi_{TM} - \phi_{TE})} \end{bmatrix} = e^{i\phi} \begin{bmatrix} 1 & 0 \\ 0 & e^{i\Delta\phi} \end{bmatrix}$$

example

入射光	半波片 $\sim \Delta\phi = \frac{2\pi}{2} = \pi$	四分之一波片 $\sim \Delta\phi = \frac{2\pi}{4} = \frac{\pi}{2}$
线偏 $[\downarrow]$	椭圆偏 $[2e^{i\pi}]$ (一般)	椭圆偏 $[2e^{i\frac{\pi}{2}}]$ (一般)
圆偏 $[\uparrow]$	椭圆偏 $[e^{i\pi}]$	线偏 $[e^{i\frac{\pi}{2}}] \sim [-1]$
椭圆偏	椭圆偏	椭圆偏
自然	自然	自然

# 几何光学



物理系统

光

光沿直线传播

$$\text{Snell's Law} \begin{cases} \theta_i = \theta_r \\ n_i \sin \theta_i = n_t \sin \theta_t \end{cases}$$

光学元器件

存在一个对称轴  $\Rightarrow$  光轴



傍轴近似

$$\theta \approx 0^\circ$$

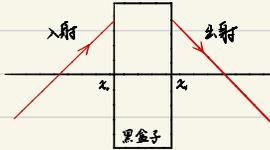
数学建模

光的建模

用最简单的一组数学完整地描述光线



光学元器件



原则

光学元器件的作用是把一束入射光变成一束出射光

$\Leftrightarrow$  建立一个从入射光  $(h_1, \theta_1)_x_1$  到出射光  $(h_2, \theta_2)_x_2$  的函数

数学模型

$$\begin{cases} h_2 = f_1(h_1, \theta_1) \\ \theta_2 = f_2(h_1, \theta_1) \end{cases} \xrightarrow[\text{线性函数}]{\text{线性近似}} \begin{cases} h_2 = ah_1 + b\theta_1 \\ \theta_2 = ch_1 + d\theta_1 \end{cases}$$

ABCD矩阵

$$\begin{bmatrix} a & b \\ c & d \end{bmatrix}$$

光学元器件由  $(a, b, c, d)$  4个数字确定

$$\begin{bmatrix} h_2 \\ \theta_2 \end{bmatrix}_{x_2} = \begin{bmatrix} a & b \\ c & d \end{bmatrix} \begin{bmatrix} h_1 \\ \theta_1 \end{bmatrix}_{x_1}$$

傍轴近似

线性近似  $(f_1, f_2)$

# 光学元器件举例

## 单个光学元器件

真空

$$\begin{bmatrix} 1 & x_1 - x_0 \\ 0 & 1 \end{bmatrix}$$

折射界面

$$\begin{bmatrix} 1 & 0 \\ 0 & \frac{n_2}{n_1} \end{bmatrix}$$

球形界面

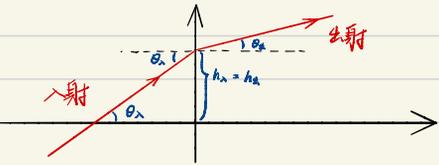
$$\begin{bmatrix} 1 & 0 \\ \frac{1}{R} \left( \frac{n_2}{n_1} - 1 \right) & \frac{n_2}{n_1} \end{bmatrix}$$

最简单的光学元器件

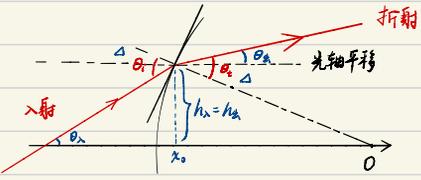


$$\begin{cases} h_o = h_i + (x_1 - x_0) \tan \theta_o \\ \theta_o = \theta_i \end{cases} \xrightarrow{\text{傍轴近似}} \begin{cases} h_o = h_i + (x_1 - x_0) \theta_i \\ \theta_o = 0 \cdot h_i + \theta_i \end{cases}$$

$\tan \theta_o \sim \theta_o$



$$\begin{cases} h_o = h_i \\ n_1 \sin \theta_i = n_2 \sin \theta_o \end{cases} \xrightarrow{\text{傍轴近似}} \begin{cases} h_o = h_i + 0 \cdot \theta_i \\ \theta_o = 0 \cdot h_i + \frac{n_1}{n_2} \theta_i \end{cases}$$

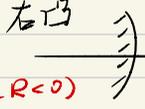


曲面曲率很小  
 $\Rightarrow R \gg$  所有特征尺寸

$$\begin{cases} h_o = h_i \\ \theta_o = \theta_i + \Delta \\ \theta_t = \theta_o + \Delta \\ \sin \Delta = \frac{h_i}{R} \xrightarrow{\text{曲率小}} \Delta = \frac{h_i}{R} \\ n_1 \sin \theta_i = n_2 \sin \theta_o \xrightarrow{\text{傍轴近似}} n_1 \theta_i = n_2 \theta_o \end{cases} \Rightarrow \begin{cases} h_o = h_i + 0 \cdot \theta_i \\ \theta_o = \frac{1}{R} \left( \frac{n_2}{n_1} - 1 \right) h_i + \frac{n_1}{n_2} \theta_i \end{cases}$$



$$\begin{bmatrix} 1 & 0 \\ \frac{1}{R} \left( \frac{n_2}{n_1} - 1 \right) & \frac{n_2}{n_1} \end{bmatrix}$$



$$\begin{bmatrix} 1 & 0 \\ \frac{1}{|R|} \left( 1 - \frac{n_2}{n_1} \right) & \frac{n_2}{n_1} \end{bmatrix}$$

组合光学元器件(共轴)

抽象系统

↓

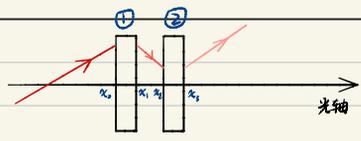
推导

↓

光元①+真空+光元②

光元①+光元②

推广



$$\begin{bmatrix} a_{12} & b_{12} \\ c_{12} & d_{12} \end{bmatrix} = \begin{bmatrix} a_2 & b_2 \\ c_2 & d_2 \end{bmatrix} \otimes \begin{bmatrix} a_1 & b_1 \\ c_1 & d_1 \end{bmatrix}$$

$$\lambda \begin{bmatrix} h_\lambda \\ \theta_\lambda \end{bmatrix} \quad \text{经过} \quad \begin{bmatrix} h_1 \\ \theta_1 \end{bmatrix}_{x_1} \rightarrow \begin{bmatrix} h_2 \\ \theta_2 \end{bmatrix}_{x_2} \quad \text{出} \quad \begin{bmatrix} h_\lambda \\ \theta_\lambda \end{bmatrix}$$

$$\begin{bmatrix} h_\lambda \\ \theta_\lambda \end{bmatrix}_{x_3} = \begin{bmatrix} a_2 & b_2 \\ c_2 & d_2 \end{bmatrix} \begin{bmatrix} h_2 \\ \theta_2 \end{bmatrix}_{x_2}$$

$$\begin{bmatrix} h_2 \\ \theta_2 \end{bmatrix}_{x_2} = \begin{bmatrix} 1 & x_2 - x_1 \\ 0 & 1 \end{bmatrix} \begin{bmatrix} h_1 \\ \theta_1 \end{bmatrix}_{x_1}$$

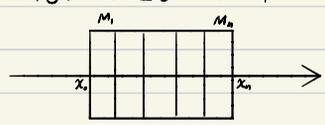
$$\begin{bmatrix} h_1 \\ \theta_1 \end{bmatrix}_{x_1} = \begin{bmatrix} a_1 & b_1 \\ c_1 & d_1 \end{bmatrix} \begin{bmatrix} h_\lambda \\ \theta_\lambda \end{bmatrix}_{x_\lambda}$$

$$\Rightarrow \begin{bmatrix} h_\lambda \\ \theta_\lambda \end{bmatrix}_{x_3} = \begin{bmatrix} a_2 & b_2 \\ c_2 & d_2 \end{bmatrix} \begin{bmatrix} 1 & x_2 - x_1 \\ 0 & 1 \end{bmatrix} \begin{bmatrix} a_1 & b_1 \\ c_1 & d_1 \end{bmatrix} \begin{bmatrix} h_\lambda \\ \theta_\lambda \end{bmatrix}_{x_\lambda}$$

$$\begin{bmatrix} a_2 & b_2 \\ c_2 & d_2 \end{bmatrix} \begin{bmatrix} 1 & x_2 - x_1 \\ 0 & 1 \end{bmatrix} \begin{bmatrix} a_1 & b_1 \\ c_1 & d_1 \end{bmatrix}$$

$$\lim_{x_1 \rightarrow x_2} (\text{光元①+真空+光元②}) \Rightarrow \begin{bmatrix} a_2 & b_2 \\ c_2 & d_2 \end{bmatrix} \begin{bmatrix} a_1 & b_1 \\ c_1 & d_1 \end{bmatrix}$$

任意共轴光学元器件的组合

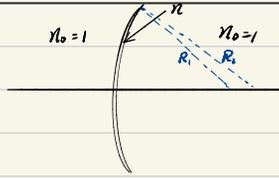


$$M_i \sim \begin{bmatrix} a_i & b_i \\ c_i & d_i \end{bmatrix}$$

$$\text{整体} \begin{bmatrix} a_{120001} & b_{120001} \\ c_{120001} & d_{120001} \end{bmatrix} = \begin{bmatrix} a_n & b_n \\ c_n & d_n \end{bmatrix} \begin{bmatrix} a_{n-1} & b_{n-1} \\ c_{n-1} & d_{n-1} \end{bmatrix} \dots \begin{bmatrix} a_1 & b_1 \\ c_1 & d_1 \end{bmatrix}$$

举例

薄凹透镜

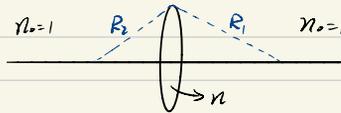


$$M_{\text{透镜}} = \begin{bmatrix} 1 & 0 \\ \frac{1}{R_1}(\frac{n}{n_0}-1) & \frac{n}{n_0} \end{bmatrix} \begin{bmatrix} 1 & 0 \\ \frac{1}{R_2}(\frac{n_0}{n}-1) & \frac{n_0}{n} \end{bmatrix} = \begin{bmatrix} 1 & 0 \\ \frac{1}{R_1}(\frac{n}{n_0}-1) & \frac{n}{n_0} \end{bmatrix} \begin{bmatrix} 1 & 0 \\ \frac{1}{R_2}(\frac{n_0}{n}-1) & \frac{n_0}{n} \end{bmatrix}$$

$$= \begin{bmatrix} 1 & 0 \\ \frac{1}{R_1}(n-1) & n \end{bmatrix} \begin{bmatrix} 1 & 0 \\ \frac{1}{R_2}(\frac{1}{n}-1) & \frac{1}{n} \end{bmatrix} = \begin{bmatrix} 1 & 0 \\ (n-1)(\frac{1}{R_1}-\frac{1}{R_2}) & 1 \end{bmatrix} = \begin{bmatrix} 1 & 0 \\ -\frac{1}{f} & 1 \end{bmatrix}$$

透镜焦距  $f = (n-1)(\frac{1}{R_1}-\frac{1}{R_2})$

薄凸透镜



$$M_{\text{透镜}} = \begin{bmatrix} 1 & 0 \\ \frac{1}{R_1}(1-\frac{n_0}{n}) & \frac{n_0}{n} \end{bmatrix} \begin{bmatrix} 1 & 0 \\ \frac{1}{R_2}(\frac{n}{n_0}-1) & \frac{n}{n_0} \end{bmatrix} = \begin{bmatrix} 1 & 0 \\ \frac{1}{R_1}(1-\frac{n_0}{n}) & \frac{n_0}{n} \end{bmatrix} \begin{bmatrix} 1 & 0 \\ \frac{1}{R_2}(\frac{n}{n_0}-1) & \frac{n}{n_0} \end{bmatrix}$$

$$= \begin{bmatrix} 1 & 0 \\ \frac{1}{R_2}(1-n) & n \end{bmatrix} \begin{bmatrix} 1 & 0 \\ \frac{1}{R_1}(\frac{1}{n}-1) & \frac{1}{n} \end{bmatrix} = \begin{bmatrix} 1 & 0 \\ (1-n)(\frac{1}{R_1}+\frac{1}{R_2}) & 1 \end{bmatrix} = \begin{bmatrix} 1 & 0 \\ -\frac{1}{f} & 1 \end{bmatrix}$$

焦距  $f = (n-1)(\frac{1}{R_1}+\frac{1}{R_2})$

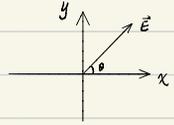
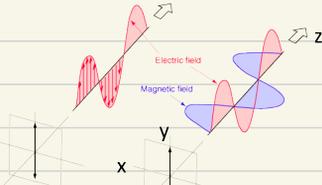
# 偏振 波函数

$$\nabla \cdot \vec{E} = \frac{1}{\mu \epsilon} \nabla \cdot \vec{E} \Leftrightarrow \begin{cases} \frac{\partial^2 E_x}{\partial x^2} + \frac{\partial^2 E_x}{\partial y^2} + \frac{\partial^2 E_x}{\partial z^2} = \mu \epsilon \frac{\partial^2 E_x}{\partial t^2} \\ \frac{\partial^2 E_y}{\partial x^2} + \frac{\partial^2 E_y}{\partial y^2} + \frac{\partial^2 E_y}{\partial z^2} = \mu \epsilon \frac{\partial^2 E_y}{\partial t^2} \\ \frac{\partial^2 E_z}{\partial x^2} + \frac{\partial^2 E_z}{\partial y^2} + \frac{\partial^2 E_z}{\partial z^2} = \mu \epsilon \frac{\partial^2 E_z}{\partial t^2} \end{cases}$$

$(E_x, E_y, E_z)$  可以取不同的波函数  
各方向无优越性

自然光(无偏振光)

线偏振光



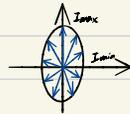
$$\begin{cases} E_x = E \cos \theta = E_0 \cos \theta e^{i(kz - \omega t)} = E_0^x e^{i(kz - \omega t)} \\ E_y = E \sin \theta = E_0 \sin \theta e^{i(kz - \omega t)} = E_0^y e^{i(kz - \omega t)} \end{cases}$$

$$\begin{bmatrix} E_x(z,t) \\ E_y(z,t) \end{bmatrix} = \begin{bmatrix} E_0^x \\ E_0^y \end{bmatrix} e^{i(kz - \omega t)} = E_0 \begin{bmatrix} \cos \theta \\ \sin \theta \end{bmatrix} e^{i(kz - \omega t)} = E_0^x \begin{bmatrix} 1 \\ \tan \theta \end{bmatrix} e^{i(kz - \omega t)}$$

琼斯矢量  $\sim \left\{ \begin{bmatrix} E_0^x \\ E_0^y \end{bmatrix}; \begin{bmatrix} \cos \theta \\ \sin \theta \end{bmatrix}; \begin{bmatrix} 1 \\ \tan \theta \end{bmatrix} \right\}$

部分偏振光

介于自然光 and 线偏光之间



偏振度  $P = \frac{I_{max} - I_{min}}{I_{max} + I_{min}}$   
 $P = 0$  (自然光/非偏振光)  
 $P = 1$  (线偏振光)

圆偏振光

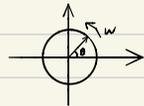
$$\begin{cases} E_x = E_0 \cos(kz - \omega t) = \text{Re}[E_0 e^{i(kz - \omega t)}] \\ E_y = E_0 \cos(kz - \omega t \pm \frac{\pi}{2}) = \text{Re}[E_0 e^{i(kz - \omega t \pm \frac{\pi}{2})}] \end{cases}$$

$$\begin{bmatrix} E_x(z,t) \\ E_y(z,t) \end{bmatrix} = E_0 \begin{bmatrix} 1 \\ e^{\pm i\frac{\pi}{2}} \end{bmatrix} e^{i(kz - \omega t)}$$

$e^{\pm i\frac{\pi}{2}}$  琼斯矢量

逆时针(左旋圆偏振光)

顺时针(右旋圆偏振光)



$$\begin{cases} E_x = E_0 \cos(kz - \omega t) \\ E_y = E_0 \sin(kz - \omega t) \end{cases} = E_0 \cos(kz - \omega t - \frac{\pi}{2})$$



$$\begin{cases} E_x = E_0 \cos(kz - \omega t) \\ E_y = -E_0 \sin(kz - \omega t) \end{cases} = E_0 \cos(kz - \omega t + \frac{\pi}{2})$$

